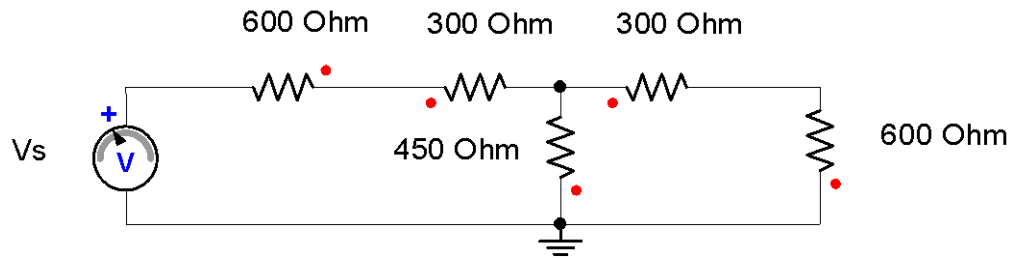
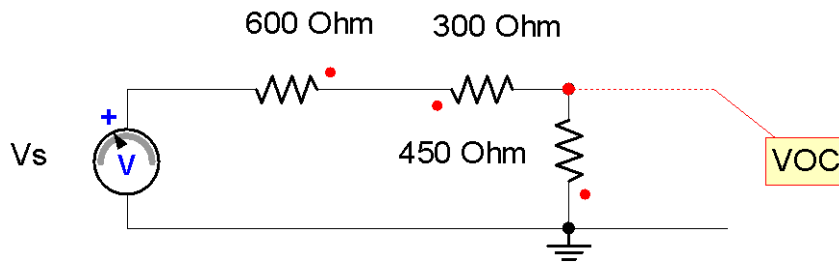


MAE140 HW3 Solutions

3.72)

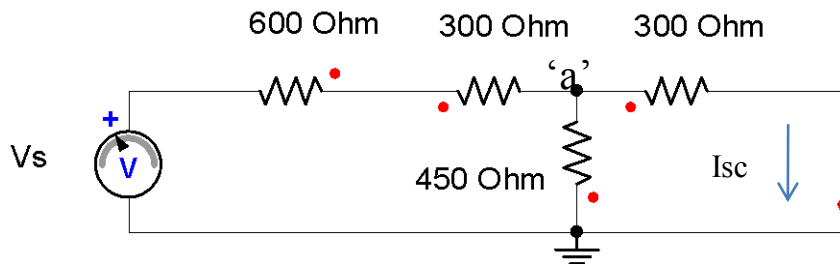


Method: Remove load resistor and find Thevenin equivalent circuit



$$V_{OC} = V_s \frac{450}{600 + 300 + 450} = \frac{V_s}{3}$$

To find I_{sc} , use a voltage divider at 'a'



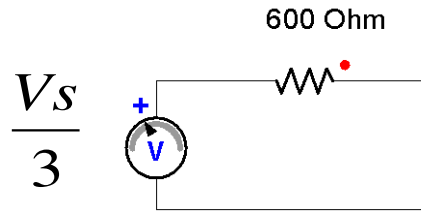
$$V_a = V_s \frac{300 \parallel 450}{300 \parallel 450 + 300 + 600} = V_s \frac{180}{180 + 900} = \frac{V_s}{6}$$

$$I_{sc} = \frac{V_a}{300} = \frac{V_s}{6 * 300} = \frac{V_s}{1800} \text{ Amps}$$

$$R_t = V_{oc} / I_{sc} = \frac{V_s / 3}{V_s / 1800} = 600 \Omega$$

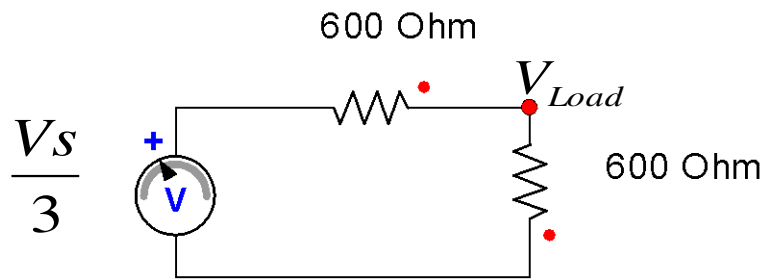
MAE140 HW3 Solutions

3.72) Continued



Thevenin Equivalent

Now put RL back to find power delivered



$$V_{Load} = \frac{1}{6} V_s \quad \text{Another voltage divider}$$

$$Power = \frac{V_{Load}^2}{R_{Load}} = \frac{V_s^2}{36 * 600} = \frac{V_s^2}{21600} \text{ Watts}$$

Without Attenuator: $V_{Load} = \frac{1}{2} V_s$

$$Power = \frac{V_{Load}^2}{R_{Load}} = \frac{V_s^2}{4 * 600} = \frac{V_s^2}{2400} \text{ Watts}$$

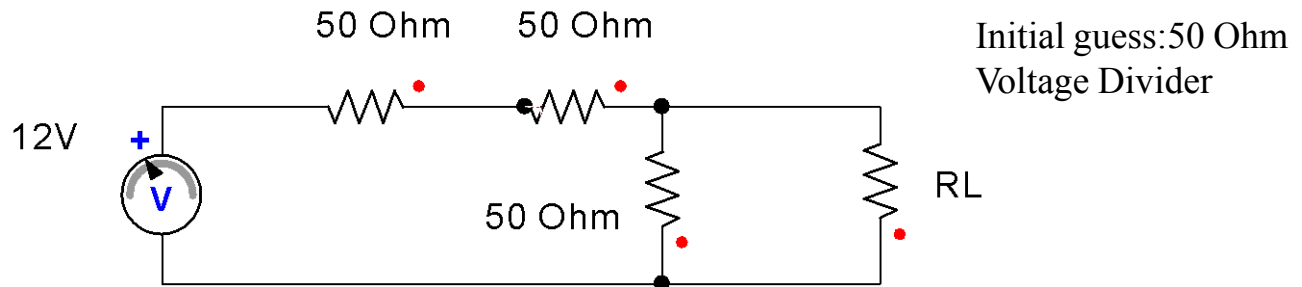
$21600/2400 = 9$: Power decreases by $1/9$

In dB $10 \log_{10} \left(\frac{V_s^2 / 21600}{V_s^2 / 2400} \right) = 10 \log_{10} \left(\frac{2400}{21600} \right) = -9.54 \text{ dB}$

For dB calculation, use $10 \log(P_a/P_b)$, not $20 \log(V_a/V_b)$ (Because power is proportional to V^2 , we use $20 \log(A/B)$ for **Voltage or Amplitude** comparisons, and $10 \log(A/B)$ for **Power** comparisons)

MAE140 HW3 Solutions

3.73)



Check boundaries, **Let $R_L = \text{infinity}$.**

Then $I = 0$ which satisfies $I \leq 100 \text{ mA}$

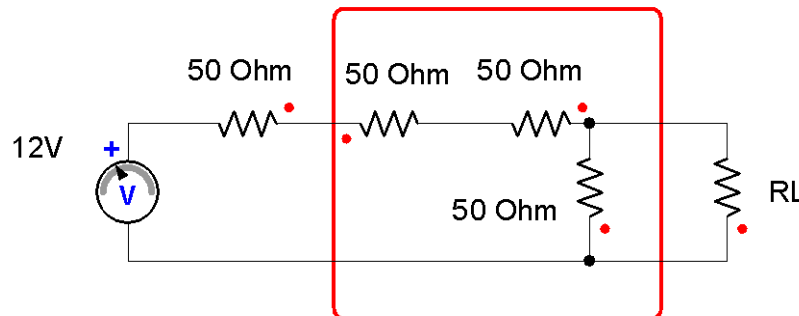
$V_L = 12 \cdot (50/150) = 4\text{V}$ which also satisfies $V_L \leq 4\text{V}$.

Note any decrease in R_L would only lower V_L so the voltage requirement will remain satisfied.

Let $R_L = 0$

$I = 12/100 = 120 \text{ mA} > 100\text{mA}$. **We need to reduce this current**

So add another series 50 Ohm to do this. This will also reduce our voltage across the load, maintaining $V_L \leq 4\text{V}$



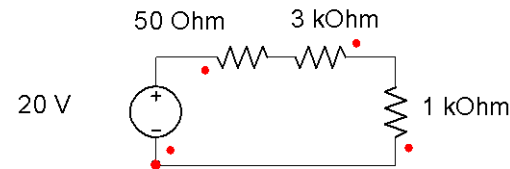
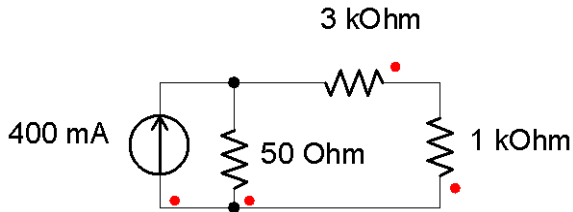
Check: V_{max} (when $R_L = \text{infinity}$) $= 12 \cdot (50/200) = 3\text{V}$

I_{max} (When $R_L = 0$) $= 12/150 = 80 \text{ mA}$

MAE140 HW3 Solutions

3.76)

Team A



It is sometimes convenient to convert to the Thevenin equivalent

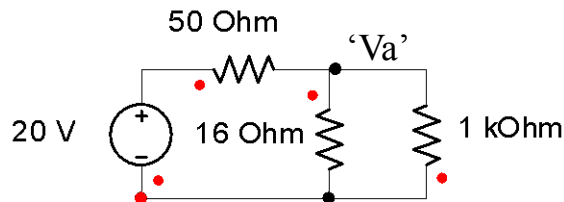
$$I = \frac{20V}{4050} = 12.345mA$$

$$P_{Load} = I^2 R_{Load} = 24.38mW$$

$$P_{Loss} = I^2 R_{3k\Omega} = 73mW$$

$$Error = \frac{25 - 24.38}{25} * 100 = 2.48\%$$

Team B



$$P_{Load} = \frac{V_a^2}{R_{Load}} = 22.9mW$$

$$P_{Loss} = \frac{V_a^2}{R_{16\Omega}} = 1.432W$$

$$Error = \frac{25 - 22.9}{25} * 100 = 8.4\%$$

Find V_a :
$$V_a = 20 * \frac{16 \parallel 1000}{50 + 16 \parallel 1000} = 20 * \frac{15.74}{50 + 15.74} = 4.788V$$

Team A clearly wins, they have

- 1) A closer tolerance
- 2) They use standard resistor values (16 Ohm isn't standard)
- 3) They waste less power (or require less power from the source)

MAE140 HW3 Solutions

3.2) (Refer to circuit drawing from HW, pg 132)

Note this circuit is linear with just resistors and independent current sources, allowing us to directly write the equations by inspection (see T,R & T pg 75)

A) **Node A:** $(1/20 + 1/10 + 1/8)V_a - 1/8 V_b = 3A$

Node B: $-1/8 V_a + (1/4 + 1/8) V_b = 1A - 3A$

Simplifying and putting into matrix form we get

$$\begin{bmatrix} \frac{11}{40} & -\frac{1}{8} \\ -\frac{1}{8} & \frac{3}{8} \end{bmatrix} \begin{bmatrix} V_a \\ V_b \end{bmatrix} = \begin{bmatrix} 3 \\ -2 \end{bmatrix} \Rightarrow \begin{bmatrix} V_a \\ V_b \end{bmatrix} = \begin{bmatrix} \frac{11}{40} & -\frac{1}{8} \\ -\frac{1}{8} & \frac{3}{8} \end{bmatrix}^{-1} \begin{bmatrix} 3 \\ -2 \end{bmatrix}$$

Computing the determinant we get $\Delta = \left[\frac{11}{40} * \frac{3}{8} \right] - \left[\frac{-1}{8} * \frac{-1}{8} \right] = .0875$

$$\begin{bmatrix} V_a \\ V_b \end{bmatrix} = \frac{1}{\Delta} \begin{bmatrix} \frac{3}{8} & \frac{1}{8} \\ \frac{1}{8} & \frac{11}{40} \end{bmatrix} \begin{bmatrix} 3 \\ -2 \end{bmatrix} = \begin{bmatrix} 10 \\ -2 \end{bmatrix}$$

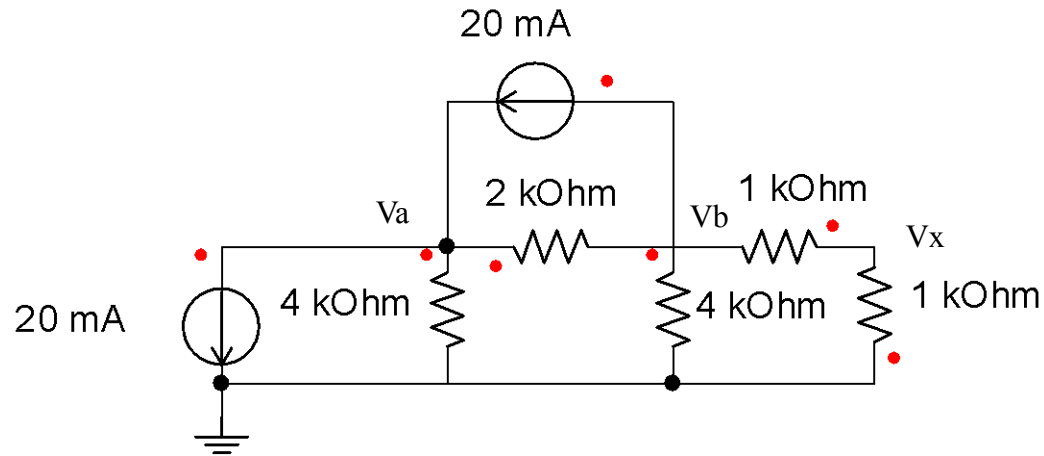
B)

$V_x = V_b = -2V$, $I_x = V_a/20 = 10/20 = 0.5 \text{ Amps}$

MAE140 HW3 Solutions

3.3)

$$\begin{aligned} \text{A)} \quad & \frac{V_a}{4k} + \frac{V_a - V_b}{2k} = 20mA - 20mA = 0 \\ & \frac{V_a - V_b}{2k} - \frac{V_b}{4k} + \frac{V_x - V_b}{1k} = 20mA \\ & \frac{V_b - V_x}{1k} - \frac{V_x}{1k} = 0 \end{aligned}$$



B) To find V_a and V_b , we can combine the two 1k resistors in series to remove a node equation, then once armed with V_b , use a voltage divider equation to get V_x .

Node A

$$\frac{V_a}{4k} + \frac{V_a - V_b}{2k} = 0 \longrightarrow \frac{3}{2} V_a = V_b$$

Node B

$$\begin{aligned} & \frac{V_b}{4k} + \frac{V_b}{2k} + \frac{V_b - V_a}{2k} = -20mA \\ & \frac{5}{4k} V_b - \frac{1}{2k} V_a = -20mA \\ & \frac{5}{4k} V_b - \frac{1}{2k} \frac{2}{3} V_b = -20mA \longrightarrow V_b = -21.8V \\ & V_a = \frac{2}{3} V_b = -14.55V \end{aligned}$$

C)

$$\begin{aligned} V_x &= V_b * \frac{1k}{1k + 1k} = -21.8 * \frac{1k}{2k} = -10.9V \\ I_x &= \frac{V_a - V_b}{2k} = \frac{-14.55 + 21.8}{2000} = 3.6mA \end{aligned}$$

MAE140 HW3 Solutions

3.4) See Figure 3-4 in HW for reference on page 132

A) By inspection, (Note V_b is known)

Node A $V_a/2k + (V_a - V_b)/4k = 1mA$

Node C $V_c/4k + (V_c - V_b)/4k = -1mA$

B) Use given values to solve for V_a and V_c

$$V_a(1/2k + 1/4k) = 1mA + 5V/4k \rightarrow V_a = 3V$$

$$V_c(2/4K) = -1mA + 5V/4k \rightarrow V_c = 0.5V$$

C) Solve for V_x and I_x ($V_b = 5V$)

$$V_x = V_a - V_c = 2.5V$$

$$I_x = (V_a - 5V)/4k + (V_c - 5V)/4k = -1.625mA$$

MAE140 HW3 Solutions

3.5) Choose ground so one side of the voltage source is connected to it (in this case, let ground be connected to $-V_s$, yielding V_c known)

A)

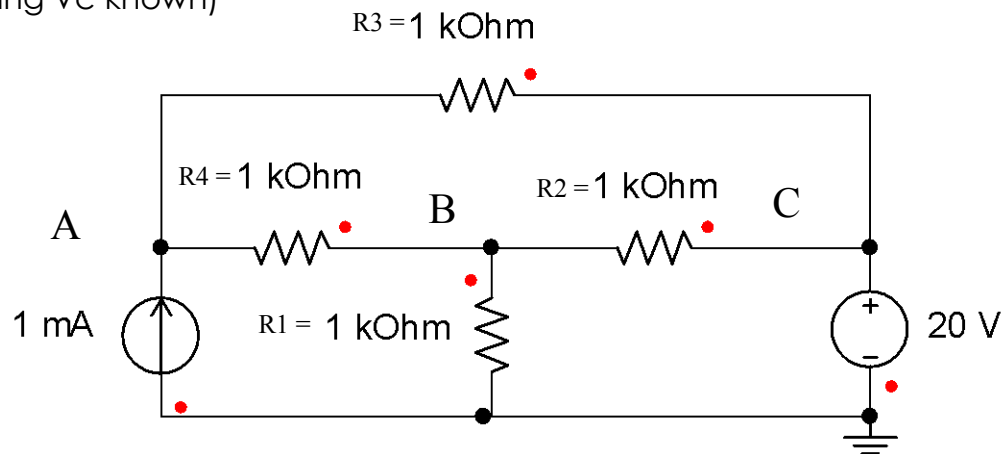
Node A $(V_a - V_c)/R_3 + (V_a - V_b)/R_2 = I_s$

Node B $(V_a - V_b)/R_4 + (V_c - V_b)/R_2 = V_b/R_1$

Since V_c is known, move it to the RHS and put node A and node B equations into matrix form

$$V_a(1/R_3 + 1/R_4) - V_b/R_4 = I_s + V_c/R_3$$

$$V_a/R_4 - V_b(1/R_4 + 1/R_2 + 1/R_1) = -V_c/R_2$$



B)

$$\begin{bmatrix} \frac{2}{1000} & \frac{-1}{1000} \\ \frac{1}{1000} & \frac{-3}{1000} \end{bmatrix} \begin{bmatrix} V_a \\ V_b \end{bmatrix} = \begin{bmatrix} 0.021 \\ -0.02 \end{bmatrix} \longrightarrow \begin{bmatrix} V_a \\ V_b \end{bmatrix} = \begin{bmatrix} 16.6V \\ 12.2V \end{bmatrix}$$

See solution 3-2 for help inverting a 2x2 matrix

$$V_x = V_b - V_c = 12.2V - 20V = -7.8V$$

$$I_x = (V_c - V_a)/R_3 = (20 - 16.6)/1k = 3.4mA$$

MAE140 HW3 Solutions

3.12)

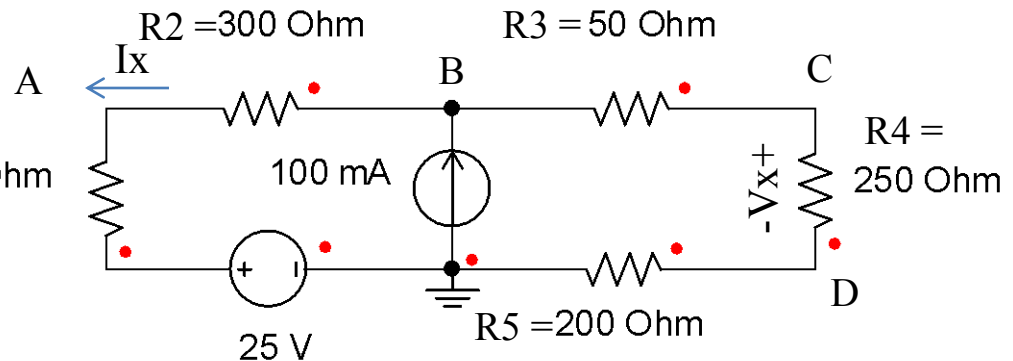
We have 4 unknown nodes

Node A: $(V_a - V_s)/R_1 - (V_b - V_a)/R_2 = 0$

Node B: $(V_b - V_a)/R_2 + (V_b - V_c)/R_3 = I_s$

Node C: $(V_b - V_c)/R_3 - (V_c - V_d)/R_4 = 0$

Node D: $(V_c - V_d)/R_4 - V_d/R_5 = 0$



To solve this circuit for V_x and I_x , we don't need to put this into a 4x4 matrix form. Instead, all we really need to find is V_b , and the whole thing will fall apart.

To do this, combine R_1 and R_2 , and combine R_3 , R_4 and R_5 . Then we get (at node B)

$(V_b - V_s)/(R_1 + R_2) + (V_b - 0)/(R_3 + R_4 + R_5) = I_s$ We can now solve for V_b directly

$(V_b - 25)/500 + V_b/500 = 100\text{mA} \rightarrow V_b = 37.5\text{V}$

Now we can compute I_x (It is flowing through R_2 and R_1) as

$(V_b - V_s)/(R_1 + R_2) = I_x \rightarrow (37.5 - 25)/500 = 25\text{ mA} = I_x$

To solve for V_x , note the current from B to C is $I_s - I_x = 75\text{ mA}$. Now just compute the $I \cdot R$ voltage drop for each resistor starting from V_b .

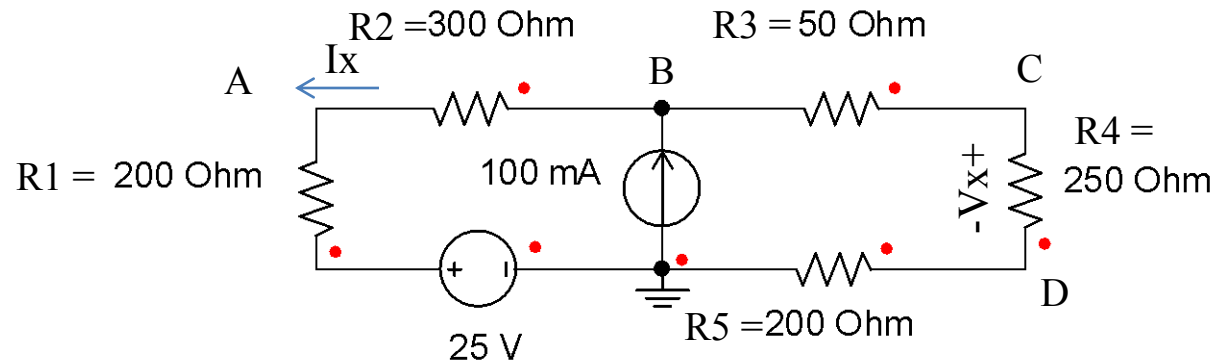
$V_c = V_b - (I_s - I_x)R_3 = 37.5 - 75\text{mA} \cdot 50 = 33.75\text{V}$

$V_d = V_c - (I_s - I_x)R_4 = 33.75 - (75\text{mA}) \cdot 250 = 15\text{V} \rightarrow V_x = V_c - V_d = 18.75\text{V}$

*You can also see that V_x must be $V_b/2$, since half the voltage is dropped across $R_3 + R_5$ and the other half is dropped across R_4

MAE140 HW3 Solutions

3.12) continued



To Find the total power dissipated in the circuit, sum the I^2R drops across each resistor plus the power dissipated by the voltage source (Current entering positive terminal means the voltage supply is dissipating power)

$$\begin{aligned} \text{Power} &= I_x^2(R1+R2) + (I_s - I_x)^2(R3+R4+R5) + I_x \cdot V_s \\ &= .025^2 \cdot 500 + .075^2 \cdot 500 + .025 \cdot 25 = \mathbf{3.75 \text{ Watts}} \end{aligned}$$

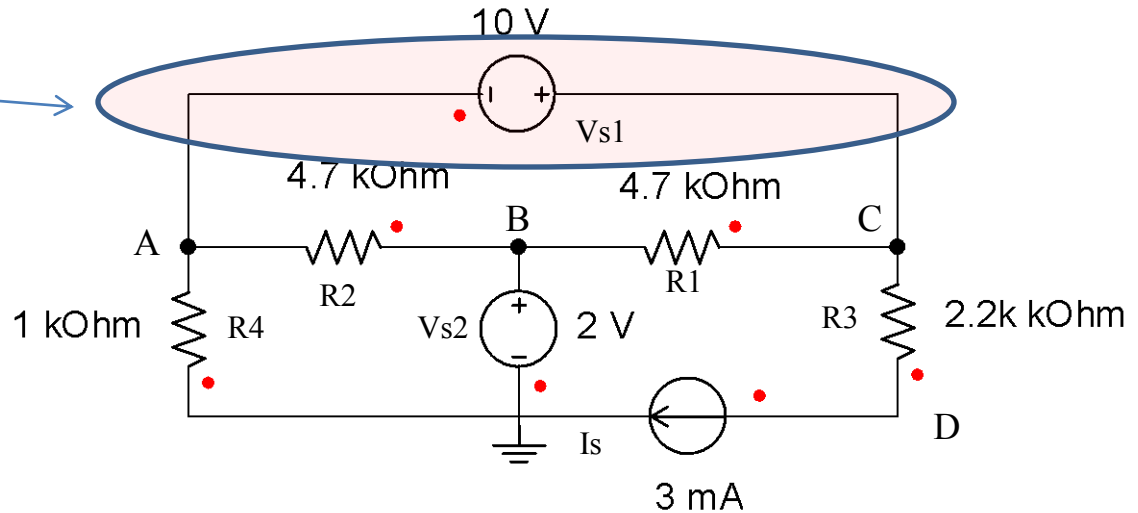
MAE140 HW3 Solutions

3.13)

Super Node

Note that if we can either find V_a or V_c , we automatically know the other one (ie $V_c = V_a + 10V$)

Also, by placing the ground as shown, we know V_b . This 4 node circuit will only require 2 equations as there are only 2 unknowns



The super node: (the sum of all currents entering the super node must be zero),

$$V_a/R_4 + (V_a - V_b)/R_2 + (V_c - V_b)/R_1 + (V_c - V_d)/R_3 = 0$$

Node D:

$$(V_c - V_d)/R_3 = I_s = 3mA$$

Using $V_b = V_{s2} = 2V$ and $V_c = V_a + 10$

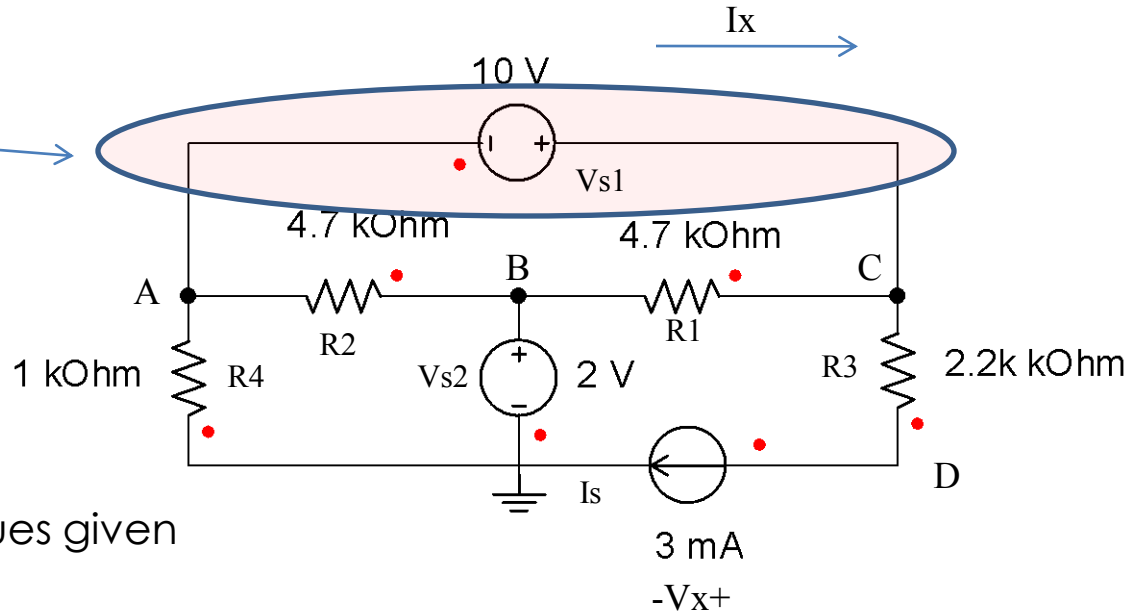
$$V_a(1/R_4 + 1/R_2 + 1/R_1 + 1/R_3) - V_d(1/R_3) = V_{s2}(1/R_1 + 1/R_2) - V_{s1}(1/R_1 + 1/R_3)$$

$$V_a/R_3 - V_d/R_3 = I_s - V_{s1}/R_3$$

MAE140 HW3 Solutions

3.13) continued

Super Node



Put into matrix form and use values given

$$\begin{bmatrix} .00188 & -.0004545 \\ .0004545 & -.0004545 \end{bmatrix} \begin{bmatrix} V_a \\ V_d \end{bmatrix} = \begin{bmatrix} -.005822 \\ -.001545 \end{bmatrix}$$

$$\begin{bmatrix} V_a \\ V_d \end{bmatrix} = \begin{bmatrix} -3 \\ .4 \end{bmatrix}$$

$$V_d = V_x = 400\text{mV}$$

$$I_x = -V_a/R_4 + (V_b - V_a)/R_2 = 4.0638\text{mA}$$

$$\text{Power supplied by } V_{s1} = I \cdot V = 10\text{V} \cdot 4\text{mA} = 40.638\text{mW}$$

MAE140 HW3 Solutions

3.14)

Refer to circuit drawing in T,R&T pg 133

Node Equations

- 1) $V_a/R_1 + (V_a - V_d)/R_6 = i_{s1}$
- 2) $-V_b/R_2 + (V_c - V_b)/R_5 = i_{s1}$
- 3) $-V_c/R_3 + (V_b - V_c)/R_6 = i_{s2}$
- 4) $V_d/R_4 + (V_d - V_a)/R_6 = i_{s2}$

To find V_x we only need V_d (place reference at $-V_x$)

So use equations 1 and 4 (2 equations, 2 unknowns, equations 2 and 3 don't have the node variables we are interested in, skip them)

$$V_a(1/R_1 + 1/R_6) + V_d(-1/R_6) = i_{s1}$$

$$V_a(-1/R_6) + V_d(1/R_4 + 1/R_6) = i_{s2}$$

You should be able to put this into matrix form and solve it by now

$$V_a = 64V$$

$$V_d = 56V = V_x$$