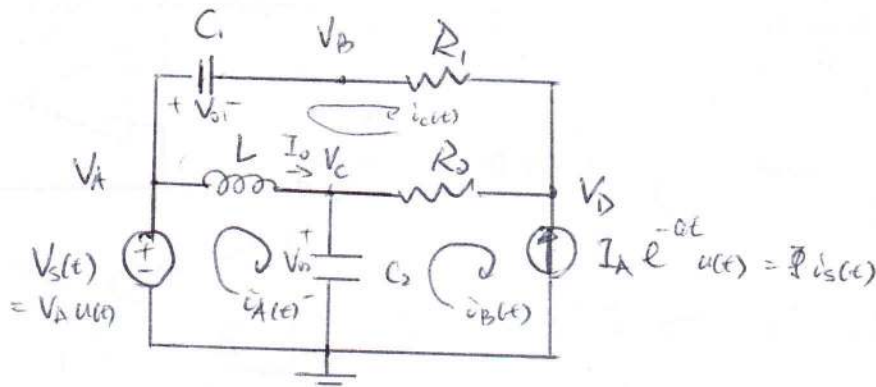
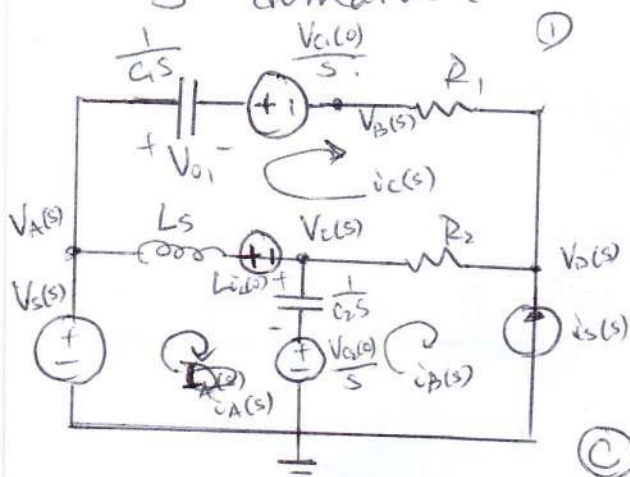


HW # 9 Solution

10.76



a) s domain:



Node Voltage: (easier w/ (2))

(A): $V_A(s) = V_C(s) = V_A \cdot \frac{1}{s}$

(B): $\frac{V_D(s) - V_B(s)}{R_1} + \frac{V_A(s) - V_B(s)}{\frac{1}{C_1 s}} - C_1 V_C(0) = 0$

(C): $\frac{V_A(s) - V_C(s)}{L s} + \frac{I_0}{s} + \frac{0 - V_C(s)}{\frac{1}{C_2 s}} + \frac{V_D(s) - V_C(s)}{R_2}$

$+ C_2 V_C(0) = 0$

(D): $\frac{V_B(s) - V_D(s)}{R_1} + \frac{V_C(s) - V_D(s)}{R_2} + i_s(s) = 0$

Mesh Current (easier w/ (1))

(1A): $V_C(s) - i_A(s) \cdot L s - L i_L(0) - (i_A(s) \cdot \frac{1}{C_1 s} - i_B(s) \cdot \frac{1}{C_2 s}) - \frac{V_C(0)}{s} = 0$

(1B): $i_B(s) = -i_s(s)$

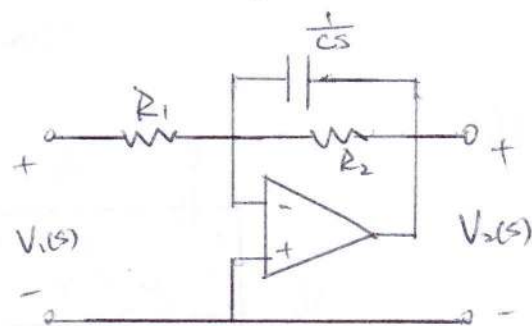
(1C): $-i_C(s) \cdot \frac{1}{C_1 s} - \frac{V_C(0)}{s} - i_C(s) \cdot R_1 - R_2(i_C(s) - i_B(s)) + L i_L(0) - L s(i_C(s) - i_A(s)) = 0$

11.6

$$a) T_V(s) = \frac{V_2(s)}{V_1(s)} = - \frac{\frac{1}{Cs + \frac{1}{R_2}}}{R_1}$$

$$= \boxed{- \frac{\frac{1}{R_1 C}}{s + \frac{1}{R_1 R_2 C}}}$$

inverting Op-Amp.



b) Input impedance $5000 \Omega \Rightarrow R_1 = 5000 \Omega$

pole: $s = - \frac{R_1}{R_1 R_2 C} = -2000 \text{ rad/s} \Rightarrow R_2 \cdot C = \frac{1}{2000} = 0.5 \text{ ms}$

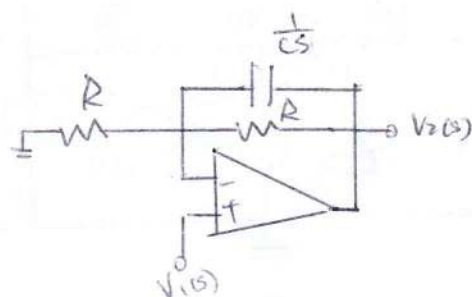
Driving point impedance:
 $Z_{in} = R_1$

$\Rightarrow \cancel{R_2 \cdot C = \frac{1}{10^3}} \cdot 10^7$ any combination s.t. $R_2 \cdot C = \cancel{10^{-7}} 2.5 \text{ s}$

11.7

$$a) T_V(s) = \frac{R + \frac{1}{Cs + \frac{1}{R}}}{R} = 1 + \frac{1}{RCs + 1} = \frac{RCs + 2}{RCs + 1}$$

$$= \frac{s + \frac{2}{RC}}{s + \frac{1}{RC}}$$



pole: $s = - \frac{1}{RC} = -2000 \text{ rad/s} \Rightarrow \text{any } R, C \text{ s.t. } RC = \frac{1}{2000} \text{ s}$

zero: $s = - \frac{2}{RC} = -4000 \text{ rad/s}$

Driving point impedance: $Z_{in} = \infty$

11.15

Assume zero initial condition

$$V_A(s) = \frac{33 \text{ k}\Omega}{\left(\frac{1}{0.056 \mu\text{F}s} + 33 \text{ k}\Omega\right)} \cdot V_1(s) \quad (\text{voltage divider})$$

$$\frac{V_2(s)}{V_A(s)} = \frac{\frac{1}{(0.1 \mu\text{F})s} + 1 \text{ k}\Omega + 10 \text{ k}\Omega}{\frac{1}{(0.1 \mu\text{F})s} + 1 \text{ k}\Omega}$$

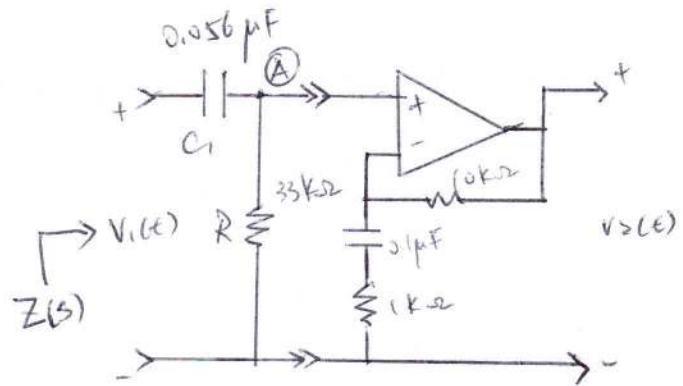
$$T_V(s) = \frac{V_2(s)}{V_1(s)} = \frac{V_2(s)}{V_A(s)} \cdot \frac{V_A(s)}{V_1(s)} = \frac{\frac{1}{0.1 \times 10^{-6}s} + 11 \times 10^3}{\frac{1}{0.1 \times 10^{-6}s} + 1 \times 10^3} \cdot \frac{33 \times 10^3}{\frac{1}{0.056 \times 10^{-6}s} + 33 \times 10^3}$$

$$= \frac{1 + 11 \times 10^{-4}s}{1 + 10^{-4}s} \cdot \frac{33 \times 0.056 \times 10^{-3}s}{33 \times 0.056 \times 10^{-3}s + 1} = \left| \frac{11(s+909) \cdot s}{(s+10^4)(s+541.13)} \right|$$

pole: $s_1 = -10^4$, $s_2 = -541.13$, Zero: $z_1 = -909$, $z_2 = 0$

Input impedance: $Z_m = \frac{V_1(s)}{\frac{V_1 - V_A}{\frac{1}{C_1 s}}}$ $V_A = \frac{33 \text{ k}\Omega}{33 \text{ k}\Omega + \frac{1}{0.056 \mu\text{F}s}} \cdot V_1$

$$Z_m = 33 + \frac{1}{0.056s}$$



11.37

$$V_2(s) = \frac{Ls}{R + \frac{1}{Cs} + Ls} V_1(s) \quad \text{assume zero IC}$$

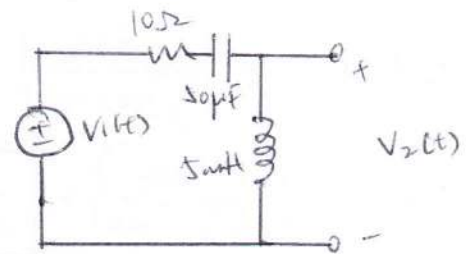
$$\frac{V_2(s)}{V_1(s)} = \frac{Ls^2}{Ls^2 + Rst + \frac{1}{C}} = \frac{s^2}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$$

$$V_2(s) = \frac{s^2}{s^2 + 2000s + 4 \times 10^6} \cdot 25 \cdot \frac{s}{s^2 + 2000} \Rightarrow V_2(t) = \mathcal{L}^{-1} \{ \dots \}$$

or $T_V = \frac{V_2(s)}{V_1(s)} = \frac{s^2}{s^2 + \frac{R}{L}s + \frac{1}{LC}}$, excited ~~the~~ system with $V_1(t) = 25 \cos(2000t) \text{ V}$

$$T_V(j2000) = \frac{-2000^2}{-2000^2 + 2000^2 j + 4 \times 10^6} \quad |T_V(j2000)| = \left| \frac{-1}{j} \right| = 1$$

$$\angle T_V(2000j) = \arg(-1) - \arg(j) = \pi - \frac{\pi}{2} = \frac{\pi}{2} \quad \therefore V_{2ss} = 25 \cos(2000t + \frac{\pi}{2}) \text{ V} = 25 \sin(2000t) \text{ V}$$



for $V_1(s) = 5V$, $\omega = 0$, $T_V(j0) = 0$

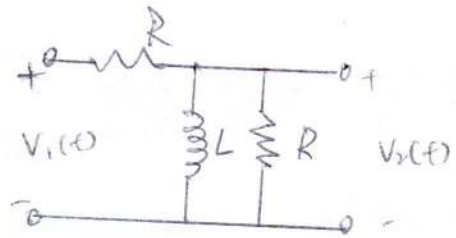
$\therefore V_2 = 0$. (By inspection, constant V_1 , then capacitor act as open circuits).

12.5

a) Voltage divider

$$\frac{V_2(s)}{V_1(s)} = \frac{\frac{1}{\frac{1}{s} + R}}{R + \frac{1}{\frac{1}{s} + R}} = \frac{1}{R(\frac{1}{s} + R) + 1}$$

$$= \frac{\frac{1}{2}s}{s + \frac{R}{2L}} = T_V(s) = \frac{1}{2} \frac{s}{s + 4700} \quad \text{High pass filter}$$



$$|T_V(j0)| = 0, \quad |T_V(j\infty)| = \left| \frac{\frac{1}{2}}{1 + \frac{R}{2L} \frac{1}{j\infty}} \right| = \frac{1}{2}, \quad \omega_{\text{cutoff}} = \left| \frac{R}{2L} \right| = 4700$$

(cutoff frequency found by $|T_V(j\omega_c)| = |T_V \max| \frac{1}{\sqrt{2}} = \frac{1}{2\sqrt{2}}$) or pole magnitude

$$c) |T_V(j\frac{1}{4}\omega_c)| = \frac{1}{2} \left| \frac{j\frac{1}{4}\omega_c}{j\frac{1}{4}\omega_c + \omega_c} \right| = \frac{1}{2} \left| \frac{j}{4+j} \right| = \boxed{\frac{1}{2\sqrt{17}}} \approx 0.1213$$

$$|T_V(j\frac{1}{2}\omega_c)| = \frac{1}{2} \left| \frac{j\frac{1}{2}\omega_c}{j\frac{1}{2}\omega_c + \omega_c} \right| = \frac{1}{2} \left| \frac{j}{2+j} \right| = \boxed{\frac{1}{2\sqrt{5}}} \approx 0.2236$$

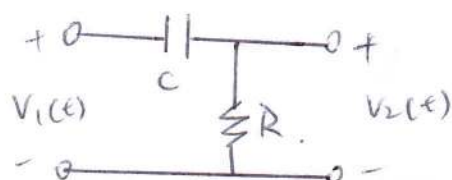
$$|T_V(j\omega_c)| = \frac{1}{2} \left| \frac{j\omega_c}{j\omega_c + \omega_c} \right| = \boxed{\frac{1}{2\sqrt{2}}} \approx 0.3536$$

12.9

high pass filter in the form of $K \frac{s}{s + \omega_c}$, $\omega_c = 159 \text{ Hz} \cdot 2\pi$

pass-band gain of 5 $\Rightarrow K = 5$

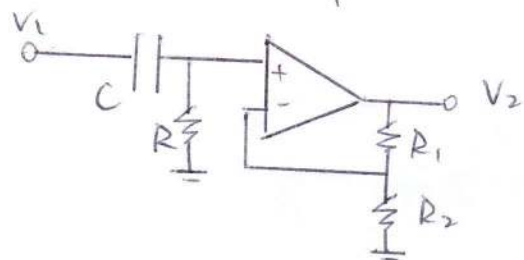
$\therefore$ high pass filter $\frac{5s}{s + \omega_c} \rightarrow$ use simplest AC circuits.



$$\frac{V_2(s)}{V_1(s)} = \frac{R}{R + \frac{1}{sC}} = \frac{CRs}{CRs + 1} = \frac{s}{s + \frac{1}{CR}}$$

select C, R s.t. $\frac{1}{CR} = \omega_c$.

what about passband gain K ? $\rightarrow$ could use Op-Amp (one choice)



select $\frac{R_1}{R_2} = 4$.

12.21

$$dB = 20 \log_{10}(\text{gain}) \Rightarrow 0 \text{ dB} \Rightarrow \text{gain} = 1.$$

low pass filter: $F(s) = \frac{\omega_c}{s + \omega_c}$ so that passband is unit gain.

$$\omega_c = 5 \text{ krad/s}. \quad |F(j\omega)| = 1 \text{ with } \omega \text{ in passband.}$$

$$|F(j500)| = \left| \frac{5000}{j500 + 5000} \right| = \left| \frac{10}{10 + j} \right| = \frac{10}{\sqrt{101}} \approx 0.995$$

as we can see, this is still w/i passband. $500 \text{ rad/s} < 5 \text{ krad/s}$. but gain is not exactly one, which is because this is the actual case, not the straight line approximation.

$$|F(j50k)| = \left| \frac{5k}{50kj + 5k} \right| = \left| \frac{1}{1 + 10j} \right| = \frac{1}{\sqrt{101}} \approx 0.0995$$

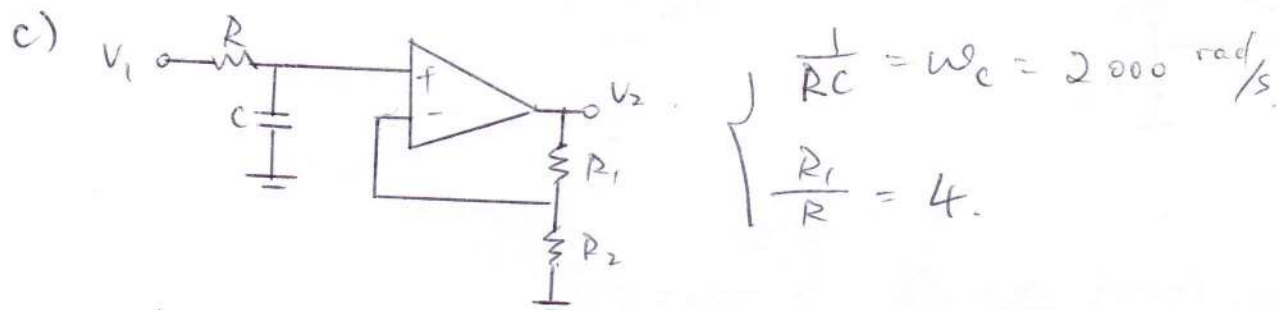
$$|F(j500k)| = \left| \frac{5k}{500kj + 5k} \right| = \left| \frac{1}{1 + 100j} \right| = \frac{1}{\sqrt{10001}} \approx 0.01$$

12.22

a) low pass filter. $\omega_c = 2000 \text{ rad/s}$, $\text{gain} = 5$

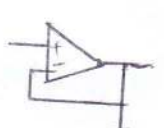
b) use matlab `tf()` command to build system, then, use

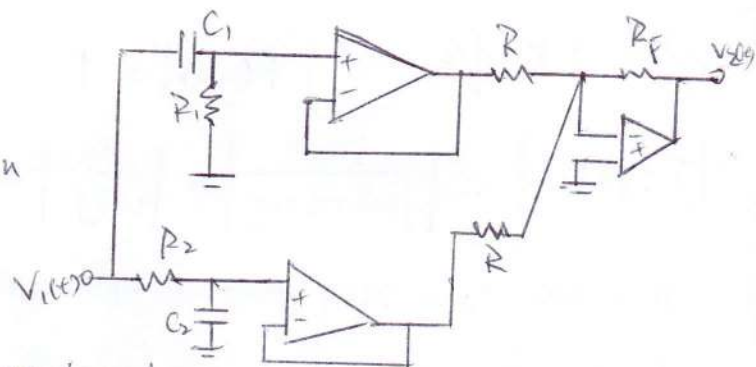
`bode()`. $\Rightarrow F = \text{tf}(10000, [1 \ 2000]);$
 $\Rightarrow \text{bode}(F)$



d) make a ω vector in matlab, then substitute $j\omega$ into transfer function $F(j\omega)$

12.34

a) the upper branch is just a ~~low~~ ^{high} pass filter $\frac{C}{R_1 + \frac{1}{s}}$, a buffer  and an inverting op-amp w/ $\text{gain} = -\frac{R_F}{R}$.



The lower branch is the same as upper branch but w/ a ~~high~~ ^{low} pass filter.

$$V_2(s) = V_{up}(s) + V_{low}(s) = -\frac{R_F}{R} \cdot \frac{R_1}{R_1 + \frac{1}{s}} V_1(s) + \left(-\frac{R_F}{R}\right) \cdot \frac{\frac{1}{C_2 s}}{R_2 + \frac{1}{s}} V_1(s)$$

$$T_V(s) = \frac{V_2(s)}{V_1(s)} = -\frac{R_F}{R} \left(\frac{s}{s + \frac{1}{R_1 C_1}} + \frac{\frac{1}{R_2 C_2}}{s + \frac{1}{R_2 C_2}} \right)$$

b). R_1, C_1, R_2, C_2 control the two cutoff frequencies. $\frac{1}{R_1 C_1}$ $\frac{1}{R_2 C_2}$
 let $\frac{1}{R_1 C_1} = 400 \text{ krad/s}$, $\frac{1}{R_2 C_2} = 4000 \text{ krad/s}$, $\omega_{center} = \frac{1}{2}(\omega_{c-LPF} + \omega_{c-HPF})$

$$|T_V(j\omega_{center})| = 40 \text{ dB} = 100. \Rightarrow \text{select } \omega_{center} \Rightarrow R_1, C_1, R_2, C_2.$$