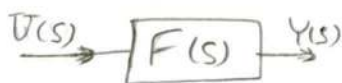


P3.16: According to the problem statement, we can consider the following block diagram:



where $U(s)$ is the Laplace transform of $u(t)$, and $Y(s)$ is the Laplace transform of $y(t)$, and $F(s)$ is the transfer function describing the associated system.

In the first part of the problem, the impulse response is given as $g(t) = e^{-t}$, $t \geq 0$. We then recall that for an impulse, $u(t) = \delta(t)$, the Laplace transform is given as $U(s) = \mathcal{L}\{\delta(t)\} = 1$, therefore, the following holds:

$$g(t) = e^{-t} \Rightarrow \mathcal{L}\{g(t)\} = Y(s) = \mathcal{L}\{e^{-t}\} = \frac{1}{s+1}$$

In addition, given the above block diagram:

$$\left. \begin{array}{l} Y(s) = U(s) F(s) \\ U(s) = 1 \end{array} \right\} \Rightarrow F(s) = Y(s) = \frac{1}{s+1} \Rightarrow \boxed{F(s) = \frac{1}{s+1} \quad (*)}$$

Thus, $(*)$ is the transfer function of the system. The order of the system is then 1 provided its # of poles. This system is also asymptotically stable, provided its only pole is $p_1 = -1 < 0$.

In order to compute the response to a constant input, $u(t) = \tilde{u}$, $t \geq 0$, we recall that:

$$u(t) = \tilde{u} \Rightarrow U(s) = \mathcal{L}\{u(t)\} = \frac{\tilde{u}}{s} \Rightarrow Y(s) = F(s) U(s) \xrightarrow[(*)]{\text{b.y.}} Y(s) = \left(\frac{1}{s+1}\right) \left(\frac{\tilde{u}}{s}\right)$$

We then split $Y(s)$ into $Y_-(s)$ and $Y_0(s)$:

$$Y(s) = \frac{\tilde{u}}{s(s+1)} = \tilde{u} \left(\frac{1}{s} - \frac{1}{s+1} \right) \Rightarrow Y(s) = \underbrace{\left(\frac{\tilde{u}}{s} \right)}_{Y_0(s)} + \underbrace{\left(-\frac{\tilde{u}}{s+1} \right)}_{Y_-(s)} \quad (**)$$

Therefore, we get:

$$y_{tr} = \mathcal{L}^{-1}\{Y_-(s)\} = \mathcal{L}^{-1}\left\{-\frac{\tilde{u}}{s+1}\right\} \Rightarrow \boxed{y_{tr}(t) = -\tilde{u} e^{-t}} : \text{transient part of the response}$$

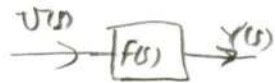
$$y_{ss} = \mathcal{L}^{-1}\{Y_0(s)\} = \mathcal{L}^{-1}\left\{\frac{\tilde{u}}{s}\right\} \Rightarrow \boxed{y_{ss} = \tilde{u} 1(t)} : \text{steady-state part of the response}$$

$$\Rightarrow y(t) = y_{tr}(t) + y_{ss}(t) \Rightarrow \boxed{y(t) = \tilde{u} (1(t) - e^{-t})} : \text{overall response}$$

$\square$

P3.17-g:

The steps to solve this problem are similar to P3.6 stated on the previous page; and thus, we state the major steps here.



$$u(t) = \delta(t) \Rightarrow U(s) = 1$$

$$y(t) = \delta(t) + t e^{-t} \sin(t) \Rightarrow Y(s) = \mathcal{L}\{\delta(t) + t e^{-t} \sin(t)\} = \mathcal{L}\{\delta(t)\} + \mathcal{L}\{t e^{-t} \sin(t)\} \quad \left. \vphantom{\mathcal{L}\{t e^{-t} \sin(t)\}} \right\} \Rightarrow$$

$$F(s) = \frac{Y(s)}{U(s)} = \mathcal{L}\{\delta(t)\} + \mathcal{L}\{t e^{-t} \sin(t)\} = 1 + H(s+1) \quad \left. \vphantom{\mathcal{L}\{t e^{-t} \sin(t)\}} \right\} \Rightarrow F(s) = 1 + \frac{2(s+1)}{(s+1)^2 + 1}$$

where $H(s) = \mathcal{L}\{t \sin(t)\} = \frac{2s}{(s^2+1)^2}$

$$\Rightarrow F(s) = \frac{(s+1)^2 + 1 + 2(s+1)}{(s+1)^2 + 1} \quad (*)$$

- The order of the system is 4, provided the order of the denominator is 4.
- The system is asymptotically stable, provided it has all its poles on the LHP, i.e., w/ negative real part.

$$\text{Let } u(t) = \tilde{u}, t \geq 0 \Rightarrow U(s) = \frac{\tilde{u}}{s} \xrightarrow{(*)} Y(s) = \frac{((s+1)^2 + 1) + 2(s+1)}{(s+1)^2 + 1} \times \frac{\tilde{u}}{s}$$

$$\Rightarrow Y(s) = \frac{((s+1)^2 + 1) + 2(s+1)}{s((s+1)^2 + 1)} \tilde{u} \Rightarrow y(t) = \mathcal{L}^{-1}\{Y(s)\} = \sum_{k=1}^3 \text{Res}(Y(s) e^{st}) \quad (**)$$

- we then have to find the partial fraction decomposition
- w/ $\left\{ \begin{array}{l} P_1 = 0, m_1 = 1, \\ P_2 = -1 + j, m_2 = 2, \\ P_3 = -1 - j, m_3 = 2, \end{array} \right.$ the next step that is surprisingly tedious can be performed now.

$$Y(s) e^{st} = \frac{((s+1)^2 + 1) + 2(s+1)}{(s+1)^2 + 1} \times \frac{\tilde{u}}{s} \times e^{st} = \left(\frac{((s+1)^2 + 1) + 2(s+1)}{(s+1)^2 + 1} \times \tilde{u} \times e^{st} \right) \frac{1}{s}$$

$$\Rightarrow \left[\text{Res}_{s=0} \{Y(s) e^{st}\} \right] = \left(\frac{((s+1)^2 + 1) + 2(s+1)}{(s+1)^2 + 1} \times \tilde{u} \times e^{st} \right) \Big|_{s=0} = \frac{4+2}{4} \times \tilde{u} \times 1 = \frac{3}{2} \tilde{u} \quad (*)$$

$$Y(s) e^{st} = \frac{((s+1)^2 + 1)^2 + 2(s+1)}{(s+1)^2 + 1)^2} \times \frac{\tilde{u}}{s} \times e^{st} = \left(\frac{((s+1)^2 + 1)^2 + 2(s+1)}{s} \times \tilde{u} \times e^{st} \right) \frac{1}{((s+1)^2 + 1)^2}$$

$$\Rightarrow \left[\text{Res} \left\{ Y(s) e^{st} \right\} \right]_{s=-1+j} = \frac{d}{ds} \left(\frac{((s+1)^2 + 1)^2 + 2(s+1)}{s} \times \tilde{u} \times e^{st} \right) \Big|_{s=-1+j} = (1-2j) \tilde{u} e^{(-1+j)t} \quad (**)$$

$$\Rightarrow \left[\text{Res} \left\{ Y(s) e^{st} \right\} \right]_{s=-1-j} = \frac{d}{ds} \left(\frac{((s+1)^2 + 1)^2 + 2(s+1)}{s} \times \tilde{u} \times e^{st} \right) \Big|_{s=-1-j} = (1+2j) \tilde{u} e^{(-1-j)t} \quad (**)$$

$y(t)$ can be obtained by plugging $(*)$, $(**)$, and $(***)$ back in $(*)$:

$$y(t) = \frac{3}{2} \tilde{u} + (1-2j) \tilde{u} (e^t (\cos t + j \sin t)) + (1+2j) \tilde{u} (e^t (\cos t - j \sin t))$$

$$\Rightarrow y(t) = \frac{3}{2} \tilde{u} + [1-2j+1+2j] \tilde{u} e^t \cos t + [j+2-j+2] \tilde{u} e^t \sin t$$

$$\Rightarrow y(t) = \frac{3}{2} \tilde{u} + 2 \tilde{u} e^t \cos t + 4 \tilde{u} e^t \sin t \quad (t)$$

Given (t) :

$$\begin{cases} y_{tr}(t) = 2 \tilde{u} e^t (2 \sin t + \cos t) \end{cases}$$

$$\begin{cases} y_{ss}(t) = \frac{3}{2} \tilde{u} \end{cases}$$



P3.24:

page 4

We refer to P 3.23 and P 3.22 where we have derived the following:

$$V_1(s) = G_T(s) T(s) + G_W(s) W(s),$$

w/

$$G_T(s) = \frac{r}{sJ + b_1 + b_2}, \text{ and } G_W(s) = \frac{r}{sJ + b_1 + b_2}.$$

In this problem we shall consider $w(t) = 0$ and thus we consider only the $T(s)$ part:

$$V_1(s) = G_T(s) T(s) = \frac{r}{sJ + b_1 + b_2} T(s)$$

Let $T(t) = \tilde{T} \cos(\omega t)$, $t \geq 0$, then the steady-state response can be computed using freq. response:

$$\text{for } T(t) = \tilde{T} \cos(\omega t) \Rightarrow V_{1,ss}(t) = \tilde{T} |G_T(j\omega)| \cos(\omega t + \angle G_T(j\omega))$$

where:

$$|G_T(j\omega)| = \left| \frac{r}{(j\omega)J + b_1 + b_2} \right| = \frac{r}{\sqrt{(J\omega)^2 + (b_1 + b_2)^2}}$$

$$\angle G_T(j\omega) = \angle \frac{r}{(j\omega)J + b_1 + b_2} = \angle r - \angle (j\omega)J + b_1 + b_2 = 0 - \tan^{-1} \left(\frac{J\omega}{b_1 + b_2} \right)$$

$$\Rightarrow V_{1,ss}(t) = \tilde{T} \frac{r}{\sqrt{(J\omega)^2 + (b_1 + b_2)^2}} \cos \left(\omega t - \tan^{-1} \left(\frac{J\omega}{b_1 + b_2} \right) \right) \quad (*)$$

Comparing (*) w/ the answer of P 3.23 which is recalled as follows:

$$V_{1,ss} = \frac{r \tilde{T}}{(b_1 + b_2)^2 + J^2 \omega^2} ((b_1 + b_2) \cos(\omega t) + J\omega \sin(\omega t)) \quad **$$

We note that (*) is the compact form of (**) and thus is easier & faster to be computed.

EB

P 3.25:

page 5

We recall the dynamics that is provided in the problem statement:

$$J\ddot{w} + \left(b + \frac{k_t k_e}{R_a}\right) \dot{w} = \frac{k_t}{R_a} v_a$$

We then compute the transfer function from v_a to w as follows:

$$\mathcal{L}\left\{J\ddot{w} + \left(b + \frac{k_t k_e}{R_a}\right) \dot{w} = \frac{k_t}{R_a} v_a\right\} \Rightarrow \mathcal{L}\left\{J\ddot{w} + \left(b + \frac{k_t k_e}{R_a}\right) \dot{w}\right\} = \mathcal{L}\left\{\frac{k_t}{R_a} v_a\right\}$$

by linearity property of Laplace:

$$\mathcal{L}\{J\ddot{w}\} + \mathcal{L}\left\{\left(b + \frac{k_t k_e}{R_a}\right) \dot{w}\right\} = \mathcal{L}\left\{\frac{k_t}{R_a} v_a\right\}$$

$$\Rightarrow sJ W(s) - Jw(0) + \left(b + \frac{k_t k_e}{R_a}\right) W(s) = \frac{k_t}{R_a} V_a(s)$$

Assuming zero-initial conditions:

$$\left(sJ + \left(b + \frac{k_t k_e}{R_a}\right)\right) W(s) = \frac{k_t}{R_a} V_a(s) \Rightarrow G(s) = \frac{W(s)}{V_a(s)} = \frac{\frac{k_t}{R_a}}{sJ + \left(b + \frac{k_t k_e}{R_a}\right)}$$

$$\Rightarrow \boxed{G(s) = \frac{W(s)}{V_a(s)} = \frac{k_t}{(R_a J)s + (bR_a + k_t k_e)}} \quad (*)$$

The only pole of (*) is $p = -\frac{bR_a + k_t k_e}{R_a J}$ which assuming all the parameters are positive is negative & thus the transfer function $G(s)$ is asymptotically stable.



P 3.27:

page 6

We recall $G(s)$ from the previous problem:

$$G(s) = \frac{w(s)}{v(s)} = \frac{k_t}{(RaJ)s + (bRa + k_t + k_e)}$$

then w/ $v_a(t) = \tilde{v}_a \cos(\omega t)$, $t \geq 0$, the steady state response using freq response technique can be obtained as follows:

$$w_{ss}(t) = \tilde{v}_a |G(j\omega)| \cos(\omega t + \angle G(j\omega)) \quad (*)$$

where

$$|G(j\omega)| = \left| \frac{k_t}{(RaJ)(j\omega) + (bRa + k_t + k_e)} \right| = \frac{k_t}{\sqrt{(RaJ\omega)^2 + (bRa + k_t + k_e)^2}} \quad (**)$$

and

$$\angle G(j\omega) = \angle \frac{k_t}{(RaJ)(j\omega) + (bRa + k_t + k_e)} = \angle k_t - \angle (RaJ)(j\omega) + (bRa + k_t + k_e)$$

$$\Rightarrow \angle G(j\omega) = -\tan^{-1} \left(\frac{RaJ\omega}{bRa + k_t + k_e} \right) \quad (***)$$

(*) by (**) & (***) yields:

$$w_{ss}(t) = \tilde{v}_a \frac{k_t}{\sqrt{(RaJ\omega)^2 + (bRa + k_t + k_e)^2}} \cos \left(\omega t - \tan^{-1} \left(\frac{RaJ\omega}{bRa + k_t + k_e} \right) \right)$$

END of HW#4 sol'n

